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Dr. Drosjack Received His B.S. Degree (Mechanical Engineering, 1970) From Carnegie-Mellon University, And His M.S. (1971) And Ph.D. (1974) Degrees (Mechanical Engineering) From The Ohio State University. He Is A Member Of ASME, The Vibration Institute, The Machinery Subcommittee Of The Ethylene Products Committee, Participates In 4th, 2024

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4.2.1 Ideal Centrifugal Flow Machines Simple Analysis Of Centrifugal Pump Or Fan Impeller Dynamics Leads To The Following Theoretical Head Relationship (Potter And Wiggert, 1997):  $H_t = \omega^2 r_2^2 / 2g - \omega \cot \beta_2 / 2\pi l_2 g Q$  (4.1) Where  $\omega$  Is The Angular Velocity Of The Impeller,  $\beta_2$  Is The Exit Blade Angle,  $R_2$  Is The 3th, 2024

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Considered An Axial Machine Thereby Neglecting Centrifugal Compressors/turbines Without Justi Cation. Also, One Might Want To Have A More Precise Relation For Design Purposes. For All These Reasons, A More Formal Derivation Is Necessary. Alexis Giauque (LMFA/ECL) Turbomachinery Aer 2th, 2024

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Also  $Dh = Cp dT = V dp$  And  $Pv = RT$ . Thus,  $P_{out} / P_{in} = T_{out} / T_{in} = Cp R / (Cp R - g)$  (9) Determining  $T_{out} = T_{in}$  From Eq. (8) And Substituting Into Eq. (9) Yields  $P_{out} / P_{in} = 1 + \frac{W}{2} \frac{Cp T_{in}}{Cp R}$  (10) Using  $Cp = 1 kJ/kg K$ ,  $T_1 = 288K$  Gives  $P_{out} / P_{in} = 2.55$  The Device Studi 3th, 2024

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